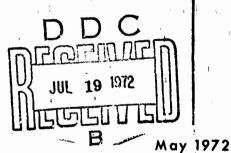
72-62-CE

COMPUTER CORRECTION OF SPECTROPHOTOMETRIC DATA

bу

M. L. Herz



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UNITED STATES ARMY
NATICK LABORATORIES
Natick, Massachusetts 01760



Clothing & Personal Life Support
Equipment Laboratory
C&PLSEL-97

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TECHNICAL REPORT 72-62-CE

COMPUTER CORRECTION OF SPECTROPHOTOMETRIC DATA

bу

M. L. Herz

Project Reference: 1T062105A349

Series: C&PLSEL-97

May 1972

Clothing and Personal Life Support Equipment Laboratory
U. S. ARMY NATICK LABORATORIES
Natick, Massachusetts 01760

FCREWORD

The utilization of computers has been widely adopted as a means of maximizing research effort in the laboratory. Many methods of calculation that are unduly complex or tedious when done by hand can be carried out with ease on a high speed computer.

The computer program presented here provides a ready method of correcting spectrophotometric data for the optical and electrical characteristics of any suitable instrument. It was prepared and utilized in the characterization of compounds in the eye protection program, but its applicability is not limited to this area. The work was carried out in the Flame and Thermal Protection section of the Chemical Modification of Textiles Branch of the Clothing and Personal Life Support Equipment Laboratory under Materials for Flashblindness Protection Project 1T062105A349 Task 05 during the period February to July 1971.

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ABSTRACT

A program was designed for correction of spectral emission data to produce the true emission spectrum. The computer output from data processed by the program consists of a tabular presentation of intensity versus wavelength or wavenumber as well as a graphical plot of the spectrum with resolution up to 2.5 nm. The computation of quantum efficiency of emission can be carried out when a reference spectrum is included in the input.

This program was written in Fortran IV for use on GE 200 Series machines. Details of use, input form, output form, and program limitations are described.

I. INTRODUCTION

The common fluorescence spectrophotometer used for the study of fluorescence and phosphorescence records "apparent emission spectra" or "relative spectral emission." Because of the non-linear response characteristics of the detector system, (Appendix B), the spectra obtained directly from the instrument are grossly distorted versions of the true spectrum. For use in such studies as fluorescence quenching, intermolecular energy transfer, fluorescence efficiencies, and fluorescence analysis, the data obtained must be expressed in terms of the actual, or true spectra. When this has been done, data from different instruments may be compared directly.

II. OBJECTIVE

The techniques used in the laboratory to calibrate spectrophotometers for source, monochromator, and detector system characteristics are described in a number of references (1). The objective of the present work is to provide a computer program which applies the overall calibration curve for the detector system to the uncorrected spectral data from a spectrofluorimeter to give the true values of the emission across the entire spectral range of the instrument. In addition, the program is designed to provide for calculation and presentation of the integrated area of the emission spectrum, a plot of the true spectrum versus wavelength or wavenumber, and the quantum efficiency of the emission.

III. DISCUSSION

Once a celibration curve, which gives the relative spectral response characteristics of the detector system for a particular instrument, is found, the adjustment of raw data to give the true spectrum involves simple calculations. The many required manipulations, being extremely tedious and repetitious, are ideal for electronic data processing.

A single computer program is presented here, which uses a given set of experimental (raw) data to compute and present the values for a number of quantities derived from emission spectra.

The computer program, (Appendix A), is written in Fortran IV in two forms, one for use with a Baird Atomic SF-1 spectrofluorimeter equipped with an RCA-Type 1P28 phototube for use in the ultraviolet

and visible spectral region, and one for use in the same instrument equipped with an RCA Type 7102, used in the near infrared region. The calibration data for these detectors are given in Appendix B.

Although the programs were written for the Baird Atomic SF-1 for its two regions of spectral sensitivity (i.e., its two detectors), the program may be used in any fluorescence spectrophotometer.

The program treats the data in four steps (Appendix C). First, the uncorrected intensity of luminescence at definite wavelength increments (the input data) is corrected and normalized. The data are first corrected by dividing the observed intensity at each wavelength of interest by the normalized spectral response at that wavelength. The corrected intensity values are then normalized by dividing by the maximum corrected intensity value found in the spectrum being measured. The normalized and corrected intensity is then known at each wavelength increment. In the second part of the program, the relative area under the corrected curve is obtained using the fourth Newton-Cotes Quadrature Formula of the closed type which gives accuracy to the fifth degree (2).

The program also provides for the calculation of the quantum efficiency of the luminescence process being studied. The luminescence intensity of a standard of known optical density (Ds) and efficiency of luminescence (Qs) is used as input along with the measured optical density of the unknown. This uncorrected spectrum of the standard is then measured under exactly the same experimental conditions (source intensity, wavelength of excitation, recorder setting, etc.) as the unknown. The intensity data of the referenced compound is then treated in the same way as the intensity data for the unknown. It is corrected, normalized, and the relative area (As) under the resulting curve is found. From this, the quantum efficiency of luminescence of the unknown (Qu) is found using the standard equation:

 $Qu = \frac{AuDs}{AsDu} \quad Qs$

where Qu = Quantum Efficiency of Unknown

Ds = Optical Density of Std.

Du = Optical Density of the Unknown

พา

(1)

Au = Area under the corrected curve of the Unknown

As = Area under the corrected curve of the Std.

Qs = Efficiency of luminescence of Std.

Finally, by means of an appropriate subroutine, the corrected spectrum is plotted against wavelength, or, if desired, wavenumber. Since the

data are stored as wavelength versus corrected intensity a plot against wavenumber necessitates the generation of a : w table which lists corrected intensity against wavenumber.

The wavelengths in the original data list are converted to a precise wavenumber, and this wavenumber is then compared to many available, uniformly incremented wavenumbers on the newly generated list. The intensity associated with the wavelength is stored with the wavenumber which is closest in value to the precise wavenumber without loss of resolution. In this way the corrected data will be listed and plotted at discrete points as intensity versus wavenumber.

In the present work, separate programs, similar except for plotting subroutines, provide different printouts of the calculated values; one program plots intensity versus wavelength; the other, intensity versus wavenumber.

Program Limitations

The Fortran IV programs can treat data for either the spectral region 300-650 nm (1P28 response) or 650-1000 nm (7102 response) with a maximum resolution of 2.5 nm. The input must be in increments of 2.5 nm or multiples thereof.

The maximum number of points in the spectral range cannot exceed 140 (350 nm spectral width). The spectral output can be plotted against wavenumber and/or wavelength depending on the subroutine used.

Input Format - from punched cards

1. Detector Calibration Curve (141 values) - FORMAT (16F5.2)

Columns

1-5, 6-10, 11-15, etc. WIA(2,I), I = 1, 141

2. Number of spectra FORMAT (I3)

1-3 NRUNS (right justified-rj)

3. Run Specification Card FORMAT (6A5,5X,415)

1-30 RUN(J), J=1,6 Run name

36-40 ISWL(rj) Initial λ (A)

	41-45	N (rj)	No. of range	points in spectral
	46-50	INC (rj)	Increm	mentation
	51-55	IND	Quantu	um yield option O=No
4.	Intensity Data	FORMAT (16)	F5 . 2)	
	1-5,6-10,11-15, etc.	ADTA(I), I	=1SWL,1	SWL+N, INC
5.	Quantum efficiency star	andard specification card		
		FORMAT (6A	5,5X,41	.5,2F5.3)
	1-30	STAND(I),	I=1 , 6	Name of reference
	36-40	IQY (rj)		Reference quantum yield
	41 - 45	IS (rj)		Initial λ ($\overset{\circ}{A}$)
	l:6 - 50	NPTS (rj)		No. of points in spectral range
	51-55	INC (rj)		Incrementation
	56-60	ODS Optio	onal	Optical density std.
ı	61 - 65	ODU		Optical density unknown
Out	put - on printer			
MAI	N PROGRAM			
	MEASUREMENT OF			
	GAVE THE FOLLOWING			
	WAVELENGTH	RESPONS	SE.	ADJ. RESPONSE
	xxx.x	XXXXXX	κχ	XXX.XXX

THE AREA UNDER THE ADJUSTED CURVE IS O.XXXXE+XX RELATIVE UNITS.

If the quantum yield calculation is indicated, then:

THE QUANTUM YIELD CALCULATED FROM THIS RUN USING A QUANTUM YIELD OF

C.XX WITH

AS A STANDARD.

THE SPECTRUM OF THE STANDARD

WAVELENGTH

RESPONSE ADJ. RESPONSE

XXXXX.X

XXXXXX.XX

XXX.XXX

THE ADJUSTED STANDARD GIVES A RELATIVE AREA OF XC.XXXXE+XX AND THE

UNKNOWN A QY OF X.XXXX.

Output Plotting Subroutines

SUBROUTINE PAWN - Wavenumber plot prints

WAVENUMBER

ADJUSTED I

XXXXX.

XXX.XX

A horizontal plot of wavenumber in increments of 50 cm⁻¹ (or 25 cm⁻¹ in the near IR) vs. adjusted intensity.

Subroutine SPLOT - Wavelength plot prints

A vertical plot of the table printed in the main program excluding the last 50 nm.

GLOSSARY OF TERMS

<u>Variable</u>	Description
WIA (1,1), I # 1,141	Wavelengths
WLA (2,1), I = 1,141	Detector calibration curve
RUN (I) , $I = 1,6$	Name of spectrum
ADTA (I)	Spectral intensities
ADJ (I)	Adjusted intensities

GLOSSARY OF TERMS (Cont'd)

STAND (I), I = 1,6 Name of reference standard

SDTA (I) Standard spectral intensities

AI An index for generating WLA (1,I)

I A general index

NI A general index (equals N + 1 SWL)

IQ A general index

J A general index

NRUNS No. of spectra

ISWL Initial wavelength

RSPEC Subroutine to adjust and normalize intensities

REL Value for largest intensity of spectrum

UREA Area under the adjusted curve of the unknown

SAREA Area under the adjusted curve of reference std.

AREA Subroutine to find the area under curve

IQΥ Integer valuε for reference quantum efficiency

IS Initial wavelength of reference spectrum

NPTS Number of points in range of reference spectrum

ODS Optical density of reference

ODU Optical density of unknown

NNI General index (equals IS + NPTS)

L General index

UQY Unknown quantum yield

IV. References

- 1. R. J. Argauer and C. E. White, Anal. Chem. 36, 368 (1964) and references cited therein.
- 2. Kaiser, K. S., "Numerical Analysis", p. 145, McGraw Hill Book Co., New York, 1957.

APPENDIX A

FORTRAN IV PROGRAMS AND SPECIMEN OUTPUT

```
$10B
SZFRO
SECRIRAN
      SPECTRUM ADJUST PROGRAM FOR AN 1P28 PHOTOTUBE WITH OPTION OF
      CALCULATING QUANTUM YIELDS DIRECTLY. INPUT CONSISTS OF UNADUST-
C
      ED SPECTRUM INTENSITIES EVERY 2.5 OR 5 NM. FROM 300 TO 650 NM.
C
      COMMON WLA
      DIMENSION WLA(2,141).RUN(6).ADTA(141).ADJ(141).STAND(141).SDTA(141
     41
    1 FORMAT(13)
    2 FORMAT(16F5,2)
    3 FORMAT [6A5,5X,415,2F5,3]
    4 FORMAT (1H1, 15HMEASUREMENT OF , 6A5/19HGAVE THE FOLLOWING -/)
    5 FORMATIZOX,10HWAVELENGTH:7X,8HRESPONSE,7X,13HADJ. RESPONSE/1
    6 FORMAT [22X,F5,1,9X,F8,2,11X,F7,3]
    7 FORMATIIHO.37HTHE AREA UNDER THE ADJUSTED CURVE IS .E11.4,15H RELA
     1TIVE UNITS
    8 FORMATIZOHTHE QUANTUM YIELD CALCULATED FROM THIS RUN USING A QUANT
     2UM YIELD OF 0., 12.1x, 5HWITH , 6A5/14HAS A STANDARD. /26X, 28HTHE SPEC
     STRUM OF THE STANDARDS
    9 FORMATI47HTHE ADJUSTED STANDARD GIVES A RELATIVE AREA OF .E11.4.1X
     3,24HAND THE UNKNOWN A DY OF ,F6,41
      AI=O.
      DO 20 1=1,141
      WLA[1:1]=300. +AI
      AI=AI+2.5
   20 CONTINUE
      READ 2.[WLA[2,1], 1=1,141]
      READ 1, NRUNS
      DO 10 IQ=1, NRUNS
      READ 3, (RUN(J), J=1,6), ISHL, N, INC, IND
      PRINT 4. [RUN[J], J=1,6]
      ISWL=[ISWL-3000]/25+1
      NI=ISWL+N
      READ 2. (ADTA(I). I=ISWLINI. INC)
      CALL RSPECIADTA, ISWL, N, ADJ, INC, REL]
      PRINT 5
      PRINTO, [WLA!1, I], ADTA(I), ADJ(I), IFISHL, NI, INC)
      UAREA = AREA (ADJ, ISHL, N, INC, REL)
      PRINT 7, UAREA
      CALL SPLOTIADJAISWLANTAINCE
      IFLIND.EQ.01GO TO 10
      READ 3, (STAND(I), I=1,61, IQY, IS, NPTS, INC. ODS, ODU
      QY=FLOAT([QY] +0.01
      IS=[IS-3000]/25+1
      NNI=IS+NPTS
      READ 2, (SDTA(L), L= IS, NNI, INC)
      CALL RSPECISDTA, IS, NPTS, ADJ, INC, REL)
      PRINT 8, IQY, (STAND(1), 1=1,6)
      PRINT 5
      PRINT 6, [WLA(1, 1), SDTA(1), ADJ(1), I= IS, NNI, INC)
      SAREA = AREA (ADJ, IS, NPTS, INC. REL1
      UQY=UAREA+QY/SAREA
```

IF CODU.NE.O..AND.ODS.NE.O.1UQY=UQY+ODS/ODU

```
END
SFORTRAN
     SUBROUTINE SPLOT(Y, ISHL, NI, INC)
     DIMENSION Y(141), IN(15), PLOT(120)
     REAL LOWER
     DATA BLANK, PLOT, POINT/121+1H ,1HX/
  81 //1
  99 FORMAT[1H1,119H I +
                        91 ////1
 100 FORMAT(120A1)
 101 FORMAT(13,4x,13,13(5x,13))
 102 FORMAT(51X,15HWAVELENGTH [NM]///]
     UPPER=100.
     LOWER#98.
     PRINT 99
     IF[NI,GT.120] NI=120
     DO 10 K=1,50
     DO 20 I=ISWL,NI,INC
     IF (Y(1), LE, UPPER, AND, Y(1), GT, LOWER) PLOT(1) = POINT
  20 CONTINUE
     PRINT 100, [PLOT[I], I=1, NI]
     DO 30 1=1,120
  30 PLOT(I)=BLANK
     UPPER#UPPER = 2.
     LOWER = LOWER = 2.
  10 CONTINUE
     DO 46 1=1,120, INC
  40 IF(Y(1), EQ.O.)PLOT(1)=POINT
     PRINT 100, [PLOT[1], [=1,120]
     DO 45 I=1,120
  45 PLOT[1]=BLANK
     IA=0
     DO 50 I=1,15
     | W[ ] = 300+ [ A
     IA=IA+20
  50 CONTINUE
     PRINT 101, [[W[]], [=1,15]
     PRINT 102
     PRINT
           98
     RETURN
```

PRENT 9, SAREA, UQY

DO 30 I=1,141

30 ADJ[I]=0, 10 CONTINUE STOP

END

```
REAL FUNCTION AREALT, ISHL, M, INC, RELI
      DIMENSION Z[141], T[141]
      NISISWL+M-1
      N = 0
      DO 10 J=ISWL,NI,INC
      N=N+1
      Z[N]=T[J]
   10 CONTINUE
      H=INC
      S=0.
C
C
    NEWTON-COTES QUADRATURE FORMULA. CLOSED TYPE
C
      IF(N .LT. 5) GO TO 840
C
           FIVE POINT FORMULA
      DO 830 1=5.N.4
      S=S+7, +Z(!-4)+32, +Z(!-3)+12, +Z(!-2)+32, +Z(!-1)+7, +Z(!)
  830 CONTINUE
      S=S+2,/45,
  840 J=N=[[N/4]+4]+1
      GO TO [845,850,847,848], J
C
           FOUR POINT FORMULA
  845 S=S+,375+(Z[N-3]+3,+Z[N-2]+3,+Z[N-1]+Z[N])
      GO TO 850
            TWO POINT FORMULA
C
  847 S=S+[Z[N-1]+Z[N]]/2.
      GO TO 850
           THREE POINT FORMULA
  848 S=S+[Z[N-2]+4,+Z[N-1]+Z[N]]/3.
  850 S=S+H
      AREA=S+REL
      RETURN
      END
SFORTRAN
      SUBROUTINE RSPECIADTA, ISHL, N, ADJ, INC. RELI
      COMMON WLA
      DIMENSION ADTA[141], WLA[2,141], ADJ[141]
      REL .
      NI=ISHL+N
DO 200 I=ISHL,NI,INC
      ADJ[1]=ADTA[1]/WLA[2,1]
      TEST=ADJ[1]
      IF (TEST, GT, REL) REL=TEST
  200 CONTINUE
      DO 210 I ISWL NI INC
      ADJ[I]=ADJ[I]*100./REL
  210 CONTINUE
      RETURN
      END
```

SLOAD

```
27,8 31, 34,5 39.6341, 43,2 49.6 53,2 55.5 59, 62,4 76, 77,2 78,5 79,9 82, 82,6 83,4 84,4 85,9 86.8 87,6
10.9114.3017. 20.5 22.
66.0568,7 70.2 72.7 74.
88,4488,7 89.1 90,3 90,8 91,4 92,1 92,4693.5 94,3 95, 95,2 94,4 93,6 92.5 90,81
90. 89, 88.4 86.0785, 83.8 82.2 80.3379.1 78. 77.2 75.8174.5 73. 71.7 70.19 69, 67.2 65.8 64.1662.8 61. 59.6 58.9656.7 55.3 54.1 51.8651.3 50.2 49.3 47.62
46,8 45,9 44.6 43,3 41,9 40,8 39,8 38,7 37.7 36.7 35.6 34,3933,6 33. 31.9 30.81
30. 28.9 28.1 26.9 25.9 24.9 24.1 22.3821.6 20.7 19.8 18.9 18.2 17.6 16.4 15.69 14.9 14. 13.4 12.3 11.7 11.1 10.5 9.5769.4 9.1 8.4 8. 7.6 7.2 6.7 6.37 6. 5.4 5.1 4.8 4.3 3.9 3.6 3.2 2.9 2.7 2.4 2.1 1.9 1.7
6.2
CARBAZOLYLACETALDEHYDE PHOS
                                                          3950
                                                                   79
3. 32, 90, 107,267, 35,5 30, 41,9 47,8 48,5 64, 76, 71, 78,5 109, 121,294, 67, 51,7 54, 57,4 56, 52,9 58, 62,8 59, 51,5 49,5 51,5 50,9 41, 32,7 26,6 24,5 24,6 24, 23,4 20, 20,9 20, 20,5 17,7 15,2
                                                        6.6 6.4 5.9 5.5 5.
1.4 1.1 1. .9 .9
3200 114 2 1
14. 13.4 13. 11.1 9. 8.2 7.
3. 2.8 2. 2. 1.9 1.7 1.4
                                                                                                 4.5
                                                                                                         4.
                                                                                                                  3.5 3.3
                                                                                                  . 9
                                                                                                          .8
                                                                                                                  . 5
 MGLN QUANTUM YIELD AT 28 16-1
                       11.3 17.1 21.5 23.9 23.8 23.1 22.1 20.4 19.1 17.2 15.3 13.5 12. 6.9 6.2 5.8 5.9 5.9 6. 6.5 7.1 7.2 7.3 7.5 7.6 7.3 5.9 5.6 5. 4.6 4.1 3.8 3.5 3.1 2.9 2.6 2.5 2.1 1.9
0. 1.5 9.9
                7,6
10,28,
7, 6,9 6,3 5,9 5,6
1,7 1,4 1,2 1,1 1.
                                       5.
                      1.1
                                                         , 9
                                                                 . 6
                                                             55 3750
QUININE SULFATE
                                                                           92
                                                                                       2.102 .044
1, 11. 25, 51, 90, 154, 203, 290, 360, 432, 528, 595, 666, 736, 770, 784, 772, 747, 710, 661, 610, 556, 501, 450, 408, 342, 302, 259, 230, 194, 167,
                                51,
142, 121, 102, 87, 64, 42, 34, 31, 26, 17, 10, 9,
```

MEASUREMENT OF CARBAZOLYLACETALDEHYDE PHOS GAVE THE FOLLOWING-

WAVELENGTH	RESPONSE	ADJ. RESPONSE
395.0	ġ , ḡ o	0.000
397.5	0.00	0.000
400.0	0.00	0.000
402,5	0,00	0.000
405.0 407.5	0,00	0.000 2.007
410.0	3,00 32,00	21.592
412,5	90,00	61.247
415,0	107,20	73.819
417.5	67.00	46.995
420.0	35.50	25.125
422,5	30.00	21.471
425.0	41.90	30.191
427.5	47.80 48.50	35.375 36.344
430.0 432.5	64,00	48.646
435.0	76.00	58.892
437,5	71.00	56.298
440.0	78,50	63.213
442.5	109.00	89.012
445.0	121.20	100.000
447,5	94.00	78.980
450.0	67,00	57.284 45.111
452,5 455,0	51.70 54.00	47.972
457,5	57,40	52.090
460.0	56.00	51.696
462,5	52.90	50.142
465.0	58,00	56.146
467,5	62.80	62.346
470,0	59.00	59.842
472.5 475.0	51.50 49.50	53.776 52.902
477.5	51.50	55.637
480.0	50,90	57.181
482,5	41.00	47.225
485.0	32.70	38.500
487,5	26.60	32.671
490.0	24.50	30.420
492,5	24.60	31.214
495.0 497.5	24,00 23,40	31.008 31.300
500.0	20.00	27.221
502.5	20.90	29.003
505.0	20,00	28.563
507.5	20,50	30.156
510,0	17,70	26.908
512.5	15.20	23.730 22.406
515.0 517.5	14.00 13.40	22.055
520,0	13.00	21.964
522,5	11.20	19.265
525.0	9,00	16.103
527,5	8.20	15.188
530,0	7.00	13.270
532.5	6.60	12.739 12.779
535,0 537,5	6,40 5,90	12.779
540,0	5,50	11.678
• -	•	

542,5	5,00	11.020
545.0	4,50	10.200
547.5	4,00	9.472
550.0	3,50	8.608
552,5	3,30	8.442
555,0	3,00	7.929
557.5	ź. 8 0	7.969
560.0	2.Ô0	5.898
562.5	ž • 0 0	6.154
565,0	i • 90	6.112
567.5	î,70	5.729
570,0	1,40	4.900
572.5	1.40 1.10	5.067
575.0	1,10	4.272
577.5	1.00	4.060
580,0	0.90	3.847
582,5	0,90	4.095
585.0	ğ•90	4.278
587.5	0.80	4.143
590.0	0.50	2.722
592,5	0,00	0.000

THE AREA UNDER THE ADJUSTED CURVE IS 0.3558E+04 RELATIVE UNITS

MEASUREMENT OF MGLN QUANTUM YIELD AT 28 16-1 GAVE THE FOLLOWING-

WAVELENGTH	F	RESPONSI		DJ.	RESPONSE
320,0		0.00			0.000
325,0	•	1.50		1	0.751
330.0	'	9,90			7.618
335,0		11.30			9.301
340.0		17.10			0.160
345,0		21.50			4.828
350,0		23,90		10	0.000
355.0		23.80			75.454
360,0		23.10			9.516
365.0 370.0		22.10			12.841 14.838
370.0 375.0		20.40			
380.0		17.20			8.131 0.216
385.0	:	15.30			3.168
390.0		13.50			6.034
395,0		12.00			0.342
400.0		10,20			33.777
405,0		8,00			6.074
410.0		7,60			4.927
415.0		6.90			23.096
420.0		0.20			21.330
425.0		5.80			0.315
430.0 435.0		5,90 5,90			21.492 2.224
440.0		6.00			3.486
445.0	•	6.50			26.069
450.0		7.10			9.508
455.0		7.20			31.092
460,0	1	7.30			32.757
465.0		7.50			55.291
470.0		7.60			37.470
475.0		7.30		3	7 . 924
480,0		7.00			8.225
485.0		6,90			39.490
490.0 495.0		6.30 5.90		,	88.024 87.054
500.0	t	5,60			37.049
505.0		5.00			34.711
510,0		4.60			3.992
515.0		4.10		3	1.896
520.0		3.80			1.209
525.0		3,50			0.441
530,0		3.10			8.566
535.0	:	2.90			8.148
540.0		5.40			6.834
545.0 550.0		2.50			?7.347 ?5.105
555.0·		1.90			24.410
560.0		1.70			4.369
565,0		1.40			1.893
570.0		1.20		2	0.415
575,0		1.10			0.767
580.0	1	1.00		2	0.780
585.0		0.90			7 .796
590,0		0.90			3.817
595 ₁ 0.		0.90			6.539
600.0 605.0		0.60		1	9.763 0.000
THE AD HISTED	CHEVE		1300E±04	DEL	

THE AREA UNDER THE ADJUSTED CURVE IS 0.1390E+04 RELATIVE UNITS

THE QUANTUM YIELD CALCULATED FROM THIS RUN USING A QUANTUM YIELD OF 0.55 WITH QUININE SULFATE AS A STANDARD.

THE SP	ECTRUM OF THE	STANDARD
WAVE', ENGTH	RESPONSE	ADJ. RESPONSE
375,0	0.00	0.000
380.0	1.00	0.100
385,0	11.00	1.087
390.0	25.00	2.425
395,0	51.00	4.878
400.0	90.00	8.479
405,0	154.00	14.279
410.0 415.0	203.00 290.00	18.942 27.616
420.0	360.00	35.234
425.0	432.00	43.046
430.0	528.00	54.717
435.0	595.00	63.760
440.0	666.00	74.166
445,0	736.00	83.978
450.0	770.00	91.042
455.0 460.0	784.00	96.317 98.554
465.0	772.00 747.00	100.000
470.0	710.00	99.587
475.0	661.00	97,692
480.0	610.00	94.766
485,0	556.00	90.528
490.0	501.00	86.025
495.0	450.00	80.403
500,0 505,0	408,00	76.793 67.546
510,0	342.00 302.00	63.489
515.0	259.00	57.322
520.0	230.00	53.739
525,0	194.00	48.002
530.0	167.00	43.781
535.0	142.00	39.211
540.0	121.00	35.528
545.0	102.00	31.974
550,0	87.00	29.589
555.0 560.0	64.00 42.00	23. 3 92 17.128
565.0	34.00	15.126
570.0	31.00	15.004
575.0	26.00	13.965
580.0	17.00	10.050
585.0	10.00	6.574
590.0	9.00	6 • 776
595,0	8,00	6.711
600.0	6.00	5.622
605.0	0.00	0.000

THE ADJUSTED STANDARD GIVES A RELATIVE AREA OF 0.4620E+05 AND THE UNKNOWN A QY OF 0.0384

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$J08
SZERO
SFORTRAN
   FOR WORK IN THE NEAR INFRARED ON THE BAIRD SF-1
      SPECTRUM ADJUST PROGRAM FOR AN IR PHOTOTUBE WITH OPTION OF
C
      CALCULATING QUANTUM YIELDS DIRECTLY.
      THE CORRECTED INTENSITY IS PLOTTED TO GIVE A PLOT OF
C
      ******WAVENUMBER VS. ADJ. INTENSITY ********
      CALCULATING QUANTUM YIELDS DIRECTLY. INPUT CONSISTS OF UNADUST-
C
      ED SPECTRUM INTENSITIES EVERY 2.5 OR 5 NM. FROM 650 TO 1000 NM.
Ç
      COMMON WLA
      DIMENSION WLA(2,141), RUN(6), ADTA(141), ADJ(141), STAND(141), SDTA(141
     41
    1 FORMAT(13)
    2 FORMAT(16F5,2)
    3 FORMAT(6A5,5X,415,2F5.3)
    4 FORMAT(1H1,15HMEASUREMENT OF ,6A5/19HGAVE THE FOLLOWING-/)
    5 FORMAT(20x,10HWAVELENGTH,7x,8HRESPONSE,7X,13HADJ. RESPONSE/)
    6 FORMAT (21X, F6, 1, 9X, F8, 2, 11X, F7, 3)
    7 FORMAT(1H0,37HTHE AREA UNDER THE ADJUSTED CURVE IS .E11.4.15H RELA
     1TIVE UNITS!
    8 FORMATI70HTHE QUANTUM YIELD CALCULATED FROM THIS RUN USING A QUANT
     2UM YIELD OF 0.,12,1x,5HWITH ,6A5/14HAS A STANDARD./26X,28HTHE SPEC
     STRUM OF THE STANDARD!
    9 FORMAT(47HTHE ADJUSTED STANDARD GIVES A RELATIVE AREA OF .E11.4.1X
     3,24HAND THE UNKNOWN A QY OF ,F6,41
   18 FORMAT(15H END OF PROGRAM)
      A1 = 0 .
      DO 20 I=1,141
      WLA(1, 1)=650. +AI
      AI=AI+2,5
   20 CONTINUE
      READ 2, [WLA(2, 1], 1=1,141]
      READ 1. NRUNS
      DO 10 IQ=1, NRUNS
      READ 3, (RUN(J), Jo1, 61, ISWL, N, INC, IND
      PRINT 4, [RUN[J], J=1,6]
      ISWL=[ISWL-6500]/25+1
      NI=ISWL+N
      READ 2. (ADTA(1), T=!SWL, NI, INC)
      CALL RSPECIADTA, ISHL, N, ADJ, INC, REL 1
      PRINT 5
      PRINTO, (KLA[1, I], ADTA[1], ADJ[I], I=ISWL, NI, INC]
      UAREA = AREA (ADJ, ISHL, N, INC, REL)
      PRINT 7, UAREA
      CALL PANNIADJ, ISHL, NI, INC.
      IFIIND.EQ.01GO TO 10
      READ 3, (STAND(11, 1=1.61, 1QY, 15, NPTS, INC, ODS, ODU
      QY=FLOAT(IQY) +0.01
      IS=[IS-6500]/25+1
      NNI=IS+NPTS
      READ 2, (SDTA(!.), L=15,NNI, INC)
      GALL RSPECISDTA, IS, NPTS, ADJ, INC, RELI
```

```
PRINT 6, [WLA[1, I], SDTA[]], ADJ[]], I=IS, NNI, INC]
      SAREA=AREA(ADJ, IS, NPTS, INC, REL)
      UQY=UAREA+QY/SAREA
      IF (ODU.NE.O..AND.ODS.NE.O.)UQY=UQY+ODS/ODU
      PRINT 9, SAREA, UQY
      no 30 1=1,141
   30 ADJ[1]=0.
   10 CONTINUE
      TYPE 18
      STOP
      END
SFORTRAN
      SUBROUTINE PAWN(ADJ, ISWL, NI, INC)
      COMMON WLA
      DIMENSION WN12,2181, WLA(2, 141), PLOT(101), ADJ(141)
      REAL LOWER
      INTEGER PLOT, BLANK, POINT
      DATA WN/436 + 0./
      DATA PLOT, BLANK, POINT/102+1H , 1HX/
    1 FORMAT(1H1,41HRELATING THESE POINTS TO WAVENUMBER GIVES/20X,10HWAV
     1ENUMBER, 7X, 10HADJUSTED I/1
    2 FORMAT(22X,F6.0.10X,F6.2.30X,[5]
    3 FORMAT(8x,2H- ,101A1,2H -)
    4 FORMATIZX, F6.0, 2X, 101A1, 2H -1
    5 FORMAT[1H1]
      CALCULATE WAVENUMBERS AND STORE IN WN
      DO 20 I=1,218
   20 WN(1, 1)=15400, -25. *FLOAT(1)
      FILL WN(2,N) WITH AVAILABLE VALUES OF ADJ
      PRINT 1
      DO 50 I=ISWL, NI, INC
      TEST=1.E07/WLA(1,I)
      DO 30 J=1,218
      IF (ABS(TEST-WN(1,J)), LE,12,5) GO TO 40
   30 CONTINUE
      GO TO 50
   40 HN(2, J) = ADJ(1)
      JST0P#J
   50 CONTINUE
      TEST=1.E07/WLA(1,ISWL)
      DO 60 J=1,218
      IF (ABS (TEST-WN(1, J)), LE, 12.5) GC TO 70
   60 CONTINUE
      J = 218
   70 JSAVE=J
      PRINT WAVENUMBERS AND ADJUSTED INTENSITIES
      DO 80 J=JSAVE, JSTOP
      IF(WN(2,J),EQ.0,1 GO TO 80
      PRINT 2. WN[1,J],WN[2,J]
   80 CONTINUE
```

21

PRINT 8, IQY, (STAND[1], I=1,6]

PRINT 5

C

C

```
PRINT 5
C
      PLOT WAVENUMBER AGAINST ADJUSTED INTENSITY
      J=1
      DO 101 I=JSAVE, JSTOP
      IF(WN(2,1),EQ,0,) GO TO 106
      UPPER#0.
      DO 102 J=1,161
      UPPER=UPPER+1.
      LOWER=UPPER-1.
      IF(WN(2,1).GE,LOWER,AND.WN(2,1),LT.UPPER) GO TO 1G3
  102 CONTINUE
      J=101
  103 PLOT(J)=POINT
  106 K=[[/5]+5
      IF(I, EQ, K) PRINT 4, WN(1, I), (PLOT(IQ), IQ=1, 1011
      IF(I, NE, K) PRINT 3, (PLOT(10), 10=1,101)
  105 PLOT(J)=BLANK
  101 CONTINUE
      RETURN
      END
SFORTRAN
      REAL FUNCTION AREAIT, ISHL, M, INC, RELI
      DIMENSION 2:141], T[141]
      NI=ISWL+M-1
      N=0
      DO 10 J=ISWL, NI, INC
      N=N+1
      Z(N)=T(J)
   10 CONTINUE
      H= INC
      S=0.
C
C
    MENTON-COTES QUADRATURE FORMULA.
                                        CLOSED TYPE
C
      IF(N ,LT. 5) GO TO 840
           FIVE POINT FORMULA
C
      DO 830 1=5.N.4
      S=S+7, +Z(1-4)+32, +Z(1-3)+12, +Z(1-2)+32.+Z(1-1)+7.+Z(1)
  830 CONTINUE
      S=S+2,/45.
  840 J=N=[[N/4]+4]+1
      GO TO [845,850,847,848],J
           FOUR POINT FORMULA
  845 S=S+,375+[Z[N-3]+3,+Z[N-2]+3,+Z[N-1]+Z[N]]
      GO TO 850
           THO POINT FORMULA
  847 SES+[Z[N-1]+Z[N]]/2.
      GO TO 850
           THREE POINT FORMULA
  848 S=S+[Z[N=2]+4,+Z[N-1]+Z[N]]/3.
  850 S=S+H
      AREA=S+REL
```

COMMON WLA

TEST=ADJ[1]

DO 200 I=ISWL,NI,INC ADJ[I]=ADTA[I'/WLA[2,I]:

RELEO. NI=ISWL+N

SUBROUTINE RSPECIADTA, ISWL, N, ADJ, INC, RELI

DIMENSION ADTA(141), WLA(2,141), ADJ(141)

SFORTRAN

SEDJ

```
IF(TEST.GT.REL) REL=TEST
  200 CONTINUE
       DO 210 I=ISWL,NI,INC
       ADJ[[]=ADJ[[]+100./REL |
  210 CONTINUE
       RETURN
       END
SLOAD
15,2 14,8 14.4 14, 13,6 13,2512,9512,6512.4 12.1 11,8511.6 11,3511.1 10.9 10,6 10,4510,2 10. 9.75 9.6 9.35 9,15 9. 8,88 8.8 8.75 8.7 8.74 8.8 8.84 8.8
8,78 8,7 8,53 8,2 7.85 7,4 7, 6.6 6,25 6.
                                                           5.8 5.6 5.4 5.2
                                                                                  5.05 4.85
                                   3.85 3.75 3.65 3.65 3.45 3.35 3.26 3.15 3.05 2.95
     4,55 4,4
                 4.25 4.1 4.
2,8512,75 2,65 2.6 2.55 2.5
                                  2.45 2.4 2,53 2.35 2.3 2.25 2.2 2.15 2.15 2.1
                                               2.
2.1 2.05 2.05 2.05 2.05 2.
                                   2.
                                                           2.
                                                                 2.
                                                                       2.
                                                                             2.
                                         2.
                                                     2.
1,95 1,95 1,95 1,95 1,9 1,9 1,9 1,85 1,85 1,85 1,8 1,8 1,7 1,7 1,65 1,65 1,65 1,6 1,6 1,5 1,55 1,53 1,50 1,5 1,35 1,35 1,3 1,3 1,25 1,25 1,25 1,2 1,2 1,15 1,15 1,1
                                                                      1,8, 1,75 1,75 1,75
1,45 1,45 1,4 1,4
                                                                            1.05 1.05
                                                                       1.1
QUANTUM YLD CARBACETALD16+1C.2
                                          6700 100
                                                          2
          5.8 8.3 12,1 22,1 20,7 18,1 18, 16, 14,9 14,9 15, 15,
                                                                                   14.9514,95
15,3 15,8 15.2 15,1 14,8 14,4 14,3 13,9 :3, 12,4 12, 11, 10,2 9,1
                                                                                  8.2 7,1
    5,9 5,1 4,7 4,1 3,7 3,2 3,
                                               2,6 2.1 1.9
                                                                1.6 1.4 1.1
€,3
                                             55 6700 100
QUININE SULFATE
                                                                2.114 .264
2, 9, 22, 47, 91, 153, 239, 343, 449, 576, 675, 780, 870, 949, 994, 1017, 1001, 967, 922, 855, 794, 719, 659, 587, 527, 460, 390, 343, 297, 257, 225,
                 22.
188, 153, 121, 100, 79, 67,
                                   52.
                                         41, 31, 28, 22, 19, 13, 11, 10,
                                                   79
CARBAZOLYLACETALDEHYDE PHOS
                                          7000
                                         90, 107,267, 35,5 30, 41,9 47.8 48.5 64, 51,7 54, 57,4 56, 52,9 58, 62,8 59, 51,5
                                   32.
78,5 109, 121,294,
                                                     23.4 20.
5.9 5.5
                                                                 20.9 20.
                                                                             20.5 17.7 15.2
                                   7.
                                                     5.9
                                                                             4.
                                                                                   3.5
                             1.7
                                   1.4
      2,8 2,
                 2.
                     1.9
                                         1.4
                                                            . 9
                                                                        . 9
                                                                              . 8
                                               1.1
                                                     1.
```

MEASUREMENT OF QUANTUM YLD CARBACETALD16-10.2 GAVE THE FOLLOWING-

WAVELENGTH	RESPONSE	ADJ. RESPONSE
670,0	0.00	0,000
675,0	2,90	6.648
680.0	5,80	13.883
685.0	8,30	20.687
690,0	12.10	31.456
695,0	22.10	60.038
700,0	20.70	58.578
705.0	18.10	53.740
710.0	18,00	55.068 49.676
715.0	16,00	46.314
720.0 725.0	14.90 14.90	45.790
730.0	15,00	46.412
735.0	15.00	47.773
740.0	14.95	51.738
745.0	14.95	58.020
75 0 , 0	15,30	66.504
755.0	15.80	74.006 76.469
760.0	15,20	81.231
765.0 770.0	15.10 14.80	85.546
775.0	14.40	88.909
780.0	14,30	94.752
785 n	13.90	98.082
790.0	13.00	96.758
795,0	12,40	97.643 100.000
800,0	12,00	97.978
805.0 810.0	11.00 10.20	97.228
815,0	9,10	93.289
820.0	8.20	87.359
825.0	7.10	78.728
830,0	6.30	67.648
835.0	5,90	69.688
840.0	5.10	62.977 59.388
845.0	4.70	53.040
850,0 855,0	3,70	49.033
860,0	3,20	42.407
865.0	3.00	40.750
870.0	2.60	35.317
875.0	2.10	28.525
880.0	1,90	25.808
885.0	1.60 1.40	21.733 19.504
890 ₁ 0 8 95 10	1.10	15.325
900.0	0.90	12.868
905.0	0.80	11.439
910.0	0.60	8.811
915.0	0.40	6.037 1.500
920,0	0,10	1.509

RELATING THESE POINTS TO WAVENUMBER GIVES WAVENUMBER ADJUSTED I

14825,	6,65
14700.	6,65 13,88
14600.	20,69
14500.	31,46
14400.	60,04
14275.	58.58
14175,	53.74
14075.	55,07
13975,	49,68
13900.	46.31
13800.	45.79
13700.	46.41
13600,	47.77
13525.	51.74
13425.	58,02
13325.	66,50
13250.	74.01
13150,	76.47
13075.	81,23
12975.	85.55
12900.	88.91
12825,	94.75
12750,	98,08
12650.	96,76
12575.	97.64
12500.	100.00 97.98
12425. 12350.	97,23
12275.	93,29
12200,	87,36
12125,	78,73
12050	67,65
11975.	69.69
11900.	62,98
11825,	59.39
11775.	53,04
11700.	49.03
11625.	42.41
11550,	40.75
11500.	35,32
11425.	28,53
11375.	25.81
11300,	21,73
11225,	19,50 15,32
11175.	
11100,	12.87
11050.	11.44
11000.	8,81
10925.	6.04
10875.	1,51

14986. 14975. 14825. 14275. 14150. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775. 13775.

THE QUANTUM YIELD CALCULATED FROM THIS RUN USING A QUANTUM YIELD OF 0.55 WITH QUININE SULFATE AS A STANDARD.

| THE | SPECTRUM OF THE | STANDARD | |
|----------------|--------------------|----------|----------------------|
| HAVELENGTH | RESPONSE | ADJ. | RESPONSE |
| 670,0 | 0.00 | | 0.000 |
| 675,0 | 2.00 | | 0.092 |
| 680.0 | 9.00 | | 0.434 |
| 685,0 | 22,00 | | 1.105 |
| 690.0 | 47.00 | | 2.463 |
| 695.0 | 91.00 | | 4.984 |
| 700.0 | 153.00 | | 8.729 |
| 705,0 | 239,00 | | 4.307 |
| 710.0
715.0 | 343.00
449.00 | | 21.156
28.106 |
| 720.0 | 578.00 | | 36.222 |
| 725,0 | 675,00 | | 41.823 |
| 730.0 | 780.00 | | 48 - 659 |
| 735.0 | 870.00 | | 55.864 |
| 740.0 | 949,00 | | 56.215 |
| 745,0 | 994,00 | | 77.777
89.125 |
| 750.0 | 1017.00
1001.00 | | 94.529 |
| 755,0
760,0 | 967.00 | | 98.083 |
| 765.0 | 927.00 | | 00.000 |
| 770.0 | 855.00 | | 99.639 |
| 775.0 | 794.00 | | 98.839 |
| 780.0 | 719.00 | | 96 - 052
93 - 753 |
| 785,0
790,0 | 659,00
587,00 | | 88.086 |
| 795.0 | 527.00 | | 83.667 |
| 800.0 | 460.00 | | 77.286 |
| 805.0 | 390.00 | | 70 - 037 |
| 810,0 | 343,00 | | 65.919 |
| 815.0 | 297.00 | | 61.386 |
| 820.0 | 257.00 | | 55.202
50.301 |
| 825,0 | 225,00
188,00 | | 40.700 |
| 830.0
835.0 | 153.00 | | 36.435 |
| 840.0 | 121,00 | | 30.125 |
| 845.0 | 100.00 | | 25.475 |
| 850,0 | 79.00 | | 20.605 |
| 855,0 | 67,00 | | 17.901 |
| 860.0 | 52,00 | | 13.893 |
| 865.0 | 41.00 | | 11.228
8.490 |
| 870.0 | 31.00 | | 7.668 |
| 875.0
880.0 | 28.00
22.00 | | 6.025 |
| 885,0 | 19,00 | | 5.203 |
| 890.0 | 13.00 | | 3.651 |
| 895.0 | 11.00 | | 3.090 |
| 900,0 | 10.00 | | 2.883 |
| 905.0 | 5.00 | | 1.441 |
| 910.0 | 0.00 | | û uuû |
| 915,0 | 0.00 | | 0.000 |
| 920,0 | 0,00 | | 0.000 |

920.0 0.000
THE ADJUSTED STANDARD GIVES A RELATIVE AREA OF 0.7182E+06 AND THE UNKNOWN A QY OF 0.0066

| WAVELENGTH | RESPONSE | ADJ, RESPONSE |
|----------------|-----------------|------------------|
| 700.0 | 0.00 | 0.000 |
| 702,5 | 0.00 | 0.000 |
| 705.0 | 0.00 | 0.000
0.000 |
| 707.5
710.0 | 0.00
0.00 | 0.000 |
| 712,5 | 3,00 | 1.758 |
| 715.0 | 32.00 | 18.859 |
| 717.5 | 90.00 | 53.346
63.250 |
| 720.0
722.5 | 107.20
67.00 | 39.262 |
| 725,0 | 35,50 | 20.709 |
| 727,5 | 30,00 | 17.580 |
| 730.0
732.5 | 41.90
47.80 | 24.609
28.333 |
| 735.0 | 48.50 | 29.320 |
| 737,5 | 64,00 | 40.248 |
| 740.0 | 76.00 | 49.925
49.477 |
| 742,5
745,0 | 71.00
78.50 | 57.829 |
| 747,5 | 109,00 | 85.165 |
| 750.0 | 121.20 | 100.000 |
| 752,5
755,0 | 94.00
67.00 | 80.789
59.570 |
| 757,5 | 51.70 | 47.608 |
| 760,0 | 54.00 | 51.568 |
| 762,5 | 57,40 | 56.923
57.184 |
| 765.0
767.5 | 56.00
52.90 | 56.246 |
| 770.0 | 58,00 | 63.637 |
| 772,5 | 62,80 | 71.175 |
| 775.0 | 59.00
51.50 | 69.148
62.488 |
| 777,5
780,0 | 49,50 | 62.259 |
| 782,5 | 51.50 | 66.393 |
| 785.0 | 50.90 | 68.176
56.381 |
| 787,5
790,0 | 41.00
32.70 | 46.199 |
| 792.5 | 26,60 | 38.639 |
| 795.0 | 24.50 | 36.621 |
| 797,5 | 24,60
24,00 | 37.868
37.964 |
| 800,0
802,5 | 23,40 | 38.307 |
| 805.0 | 20,00 | 33.815 |
| 807,5 | 20.90 | 36.534
36.188 |
| 810.0
812.5 | 20.00
20.50 | 38.441 |
| 815,0 | 17.70 | 34.443 |
| 817.5 | 15.20 | 30.147 |
| 820,0
822,5 | 14.00
13.40 | 28.312
27.640 |
| 825,0 | 13.00 | 27.362 |
| 827,5 | 11,10 | 23.850
18.344 |
| 830,0
832,5 | 9,00
8,20 | 17.994 |
| 835.0 | 7.ñ0 | 15.595 |
| 837,5 | 6.60 | 15.127 |
| 840.0
842.5 | 6.40
5.90 | 15.002
14.151 |
| 845.0 | 5,50 | 13.192 |

| 847,5 | 5.00 | 12.278 |
|-------|----------|--------|
| 850.0 | 4,50 | 11.050 |
| 852.5 | 4.00 | 10.062 |
| | 3.50 | 8.804 |
| 855.0 | • | 8.301 |
| 857.5 | 3.30 | 4 |
| 860.0 | 3.00 | 7.546 |
| 862.5 | 2.80 | 7.219 |
| 865,0 | 2.00 | 5.157 |
| 867.5 | 2,00 | 5.157 |
| 870.0 | 1.90 | 4.899 |
| 872,5 | 1.70 | 4.383 |
| | | 3.610 |
| 875,0 | 1.40 | 14 |
| 877.5 | 1.40 | 3.610 |
| 880.0 | 1,10 | 2.836 |
| 882,5 | 1.00 | 2.578 |
| 885.0 | 0.90 | 2.321 |
| 887,5 | 0,90 | 2.321 |
| | | 2.380 |
| 890.0 | 0.90 | |
| 892,5 | n • 80 | 2.116 |
| 895,0 | 0.50 | 1.322 |
| 897.5 | ดี. จิ๋ง | 0.000 |
| J., . | • | |

THE AREA UNDER THE ADJUSTED CURVE IS 0.4619E+05 RELATIVE UNITS

RELATING THESE POINTS TO WAVENUMBER GIVES MAVENUMBER ADJUSTED I

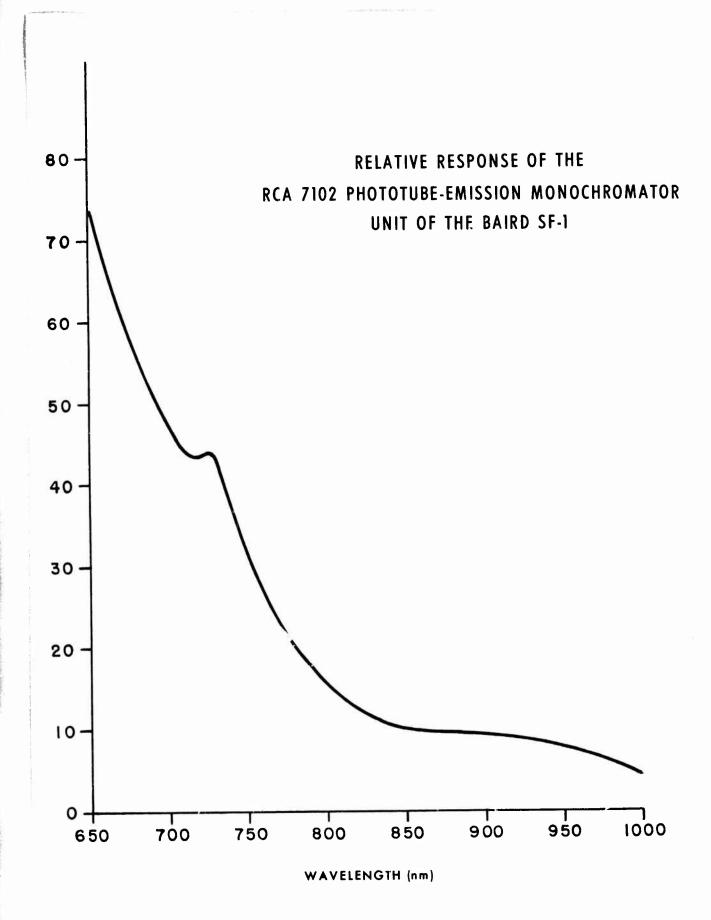
| 44025 | 4 74 |
|------------------|----------------|
| 14025. | 1,76 |
| 13975. | 18.86 |
| 13925, | 53,35 |
| 13900. | 63.25 |
| 13850, | 39,26 |
| | |
| 13800. | 20.71 |
| 13750. | 17.58 |
| 13700. | 24,61 |
| 13650. | 28,33 |
| 13650.
13600. | 29,32 |
| 13550 | 40.25 |
| 10000, | |
| 13525. | 49.93 |
| 13475. | 49.48 |
| 13425. | 57,83 |
| 43776 | 85,16 |
| | |
| 13325, | 100.00 |
| 13300. | 80.79 |
| 13250. | 59,57 |
| 13200. | 47.61 |
| 13150. | 51.57 |
| | |
| 13125. | 56.92 |
| 13075. | 57.18 |
| 13025. | 56,25 |
| 12975. | 63.64 |
| 12950. | 71.17 |
| | |
| 12900. | 69,15 |
| 12850. | 62.49 |
| 12825. | 62.26 |
| 12775. | 66,39 |
| | |
| 12750. | 68.18 |
| 12700. | 56.38 |
| 12650, | 46.20 |
| 12625. | 38,64 |
| 12575. | 36.62 |
| | |
| 12550. | 37,87 |
| 12500. | 37.96 |
| 12450. | 38.31 |
| 12425. | 33,81 |
| 12375. | 36.53 |
| | |
| 12350. | 36.19 |
| 12300, | 38,44 |
| 12275, | 34.44 |
| 12225. | 30.15 |
| 12200. | 30.15
28,31 |
| | |
| 12150. | 27,64 |
| 12125. | 27.36 |
| 12075. | 23.85 |
| 12050. | 18,34 |
| 12010. | 17.99 |
| | |
| 11975. | 15.69 |
| 11950, | 15.13 |
| 11900. | 15.08 |
| 11875. | 14.15 |
| 11825. | 13.19 |
| 11800. | 12.28 |
| | |
| 11775. | 11.05 |
| 11725. | 10.06 |
| 11700. | 8,80 |
| 11650. | 8.30 |
| 11625. | 7,55 |
| | 7,22 |
| 11600. | 1,22 |
| | |

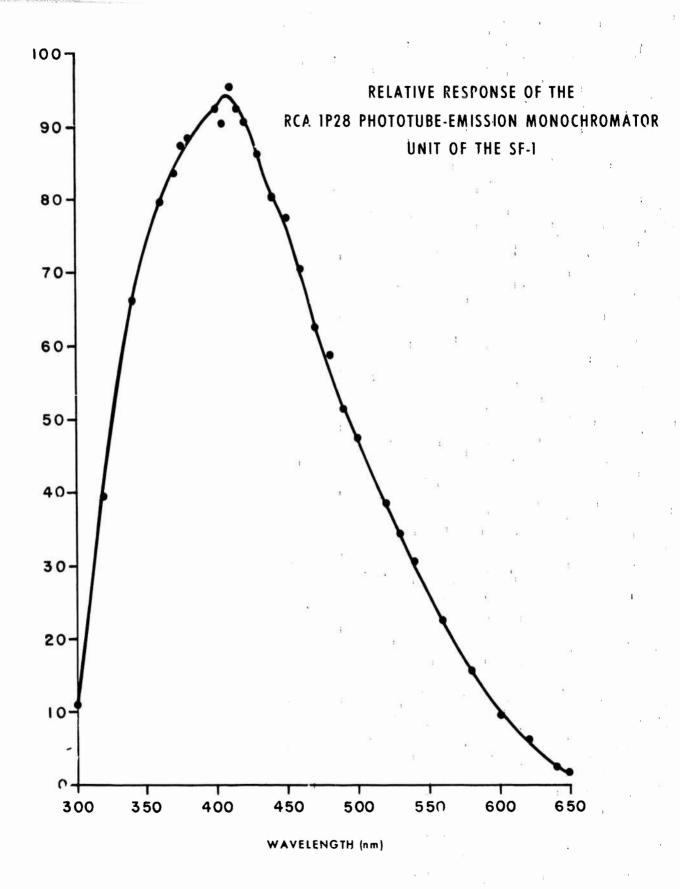
| 11550. | 5.16 |
|--------|------|
| 11525. | 5.16 |
| 11500. | 4.90 |
| 11450. | 4.38 |
| 11425, | 3.61 |
| 11400. | 3.61 |
| 11375. | 2.84 |
| 11325. | 2,58 |
| 11300. | 2.32 |
| 11275. | 2,32 |
| 11225. | 2.38 |
| 11200. | 2.12 |
| 11175. | 1.32 |
| | |

APPENDIX B

CALIBRATION CURVES

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APPENDIX C

